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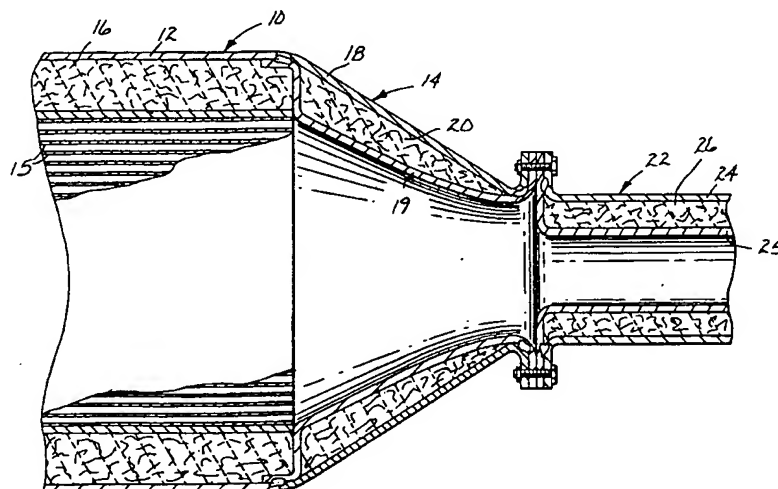
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D-81634 München (DE)(54) **Catalytic converter having a metallic monolith mounted by a heat-insulating mat of refractory ceramic fibers.**

(57) A catalytic converter (10) has a metallic monolith (15) that is mounted in a canister (12) by a heat-insulating mat (16) of melt-formed refractory ceramic fibers that have been annealed to provide a Resiliency Value of at least 10 kPa. Previously known melt-blown fibers used in such mats were thought to require a fine-grained crystalline structure to have a higher resiliency value. However, a mat in accordance with the invention having a Resiliency Value of at least 10 does not take a compression set that would allow the monolith to become loose, is made from ceramic fibers which are preferably melt-formed from a mixture of about equal parts by weight of Al_2O_3 and SiO_2 . After being annealed, the ceramic fibers can have a fine-grained crystalline structure, but significant energy savings can be realized by reducing the annealing temperatures and times such that the fibers have an amorphous structure while still attaining excellent Resiliency Values.

**EP 0 573 834 A1**

The invention concerns a catalytic converter which has a metallic monolith that is mounted by a heat-insulating blanket or mat of refractory ceramic fibers. More generally, the invention is concerned with any device that has a canister containing a metallic member and a heat-insulating blanket between the metallic member and the canister.

5 A catalytic converter typically has a metallic or ceramic monolith which is mounted within a metal canister by a heat-insulating blanket. The blanket typically is a mat of refractory ceramic fibers. In use, the monolith is heated to temperatures on the order of 600° - 1000° C while the heat-insulating mat keeps the canister at much lower temperatures. This temperature differential causes a metallic monolith to expand more than the canister, thus narrowing the gap between the monolith and the canister and compressing the
10 heat-insulating mat. Unless the mat is resilient, it can take such a compression set that the metallic monolith becomes loose when the catalytic converter cools. This would not only reduce the heat-insulating value of the mat, but in vehicular use, a loose monolith would produce annoying noises and by being buffeted would be subject to premature failure.

In addition to catalytic converters, there are other devices wherein a canister or other housing contains
15 a metallic member that becomes hot and must be insulated from the housing by a blanket or mat of refractory ceramic fibers, e.g., a diesel particulate trap, an insulated end-cone, or an insulated doublewalled exhaust pipe such as that of coassigned U.S. Pat. No. 5,024,289 (Merry). Any such heat-insulating blanket or mat should be sufficiently resilient that it does not become loose by taking a compression set when the inner metallic member expands in use to narrow the gap between the inner metallic member and its
20 housing.

A mat of refractory ceramic fibers that has sufficient resiliency to prevent a metallic monolith from becoming too loose is disclosed in coassigned U.S. Pat. Nos. 4,929,429 and 5,028,397 (both Merry). The refractory ceramic fibers used in the mat of the Merry patents can be made from an aqueous solution or a colloidal dispersion that is called an "organosol" or a "sol gel". The Merry patents say that substantially
25 shot-free ceramic fibers, formed by sol gel processes, offer the high degree of resiliency needed for mounting metallic monoliths, but that conventional ceramic fibers formed by melt processes contain shot particles and are not suitable. Comparative examples of the Merry patents show that even when melt-formed ceramic fibers have been treated to reduce the shot content to as low as 5%, they still lack the requisite resiliency. Untreated melt-formed ceramic fibers typically have shot contents within the range of
30 30 to 60%.

Refractory ceramic fibers formed by sol gel processes can be either crystalline or amorphous, depending upon the temperature at which they are fired. Those formed by conventional melt processes are initially amorphous. UK Pat. Spec. No. 1,481,133 (Johnson et al.) says that a blanket of amorphous ceramic fibers will retain a substantially permanent set under compression, but that good resiliency can be achieved
35 by converting from an amorphous form to a fine-grained crystalline form. This can be achieved by heating above the devitrification temperature of about 950° C, while avoiding higher temperatures (above about 1050° C) that would result in a coarse-grained structure.

The present invention provides a catalytic converter which, like those of the Merry '429 and '397 patents, has a monolith that is mounted in a canister by a heat-insulating mat of refractory ceramic fibers.
40 The catalytic converter of the present invention differs from that of the Merry patents in that refractory ceramic fibers of its heat-insulating mat are melt-formed and have been annealed at a temperature and for a time sufficient to provide a Resiliency Value (as defined below) of at least 10 kPa. By having such a Resiliency Value, a metallic monolith should not become loose after the heat-insulating mat has been compressed by the thermal expansion of a metallic monolith within a canister of a catalytic converter.

45 More broadly, a heat-insulating mat of annealed melt-formed refractory ceramic fibers can be employed to insulate any inner metallic member that becomes hot in use and expands to compress the mat between the metallic member and a housing.

The melt-formed refractory ceramic fibers of the heat-insulating mat can be annealed to develop a fine-grained crystalline form (as in the Johnson UK Pat. Spec.) while avoiding higher temperatures that would
50 result in a coarse-grained structure and consequently result in an unsatisfactory Resiliency Value. However, by restricting the annealing temperature and time such that the melt-formed fibers remain substantially amorphous, there is a significant energy saving as compared to Johnson's need to develop a crystalline structure.

By "substantially amorphous" is meant that no crystallinity can be detected by x-ray diffraction, even
55 though microcrystallinity has been detected in some cases by transmission electron microscopy (TEM). In experimentation to date, differential thermal analysis (DTA) shows that melt-formed refractory ceramic fibers devitrify when the annealing temperature is raised to about 990° C. X-ray diffraction shows crystallinity in those devitrified fibers, but not in identical fibers that have been annealed at temperatures lower than

990 °C.

The effectiveness of a heat-insulating mat of melt-formed refractory ceramic fibers that are substantially amorphous is surprising in view of the need in the Johnson UK Pat. Spec. to convert such fibers to a fine-grained crystalline form.

5 In view of statements in the Merry '429 and '397 patents, it is surprising that there is no need to go to the expense of treating the heat-insulating mat or its melt-formed refractory ceramic fibers to reduce or substantially eliminate shot. Good results in mounting metallic monoliths in canisters of catalytic converters have been achieved when shot comprised up to about 60% by weight of the heat-insulating mat. However, lower levels of shot are preferred when available at equivalent costs.

10 The heat-insulating mat preferably is free from materials other than annealed, melt-formed refractory ceramic fibers and preferably has only a minor proportion of binder that provides sufficient integrity to the mat to enable it to be handled and wrapped or stuffed into position in the manufacture of the device of the invention. The binder can be removed chemically after the mat is in place, or it can be burned off by the heat of the first use of the device. In the latter event, the burning binder should not emit any hazardous
15 volatiles.

A binder can be avoided by wet-laying the fibers to align most of the fibers in the plane of the heat-insulating mat, but such a mat can be difficult to handle.

The heat-insulating mat can contain additional fibers, flakes and other materials that are heat-insulating as long as they are used in proportions that do not reduce the Resiliency Value to less than 10 kPa. In
20 addition to or instead of being contained within the heat-insulating mat, such other materials can form a separate layer similar to the intumescent sheet material 32 of Fig. 3 of the Merry '429 patent. Such additional materials include unexpanded vermiculite flakes and other materials listed at col. 3, lines 28-48 of Merry '429.

A useful heat-insulating mat can be made from about 1 to 70% by weight of intumescent material,
25 about 10 to 70% by weight of annealed melt-formed refractory ceramic fibers, and about 3 to 20% by weight of binder.

The melt-formed refractory ceramic fibers can be melt-blown or melt-spun from a variety of metal oxides, preferably a mixture of Al_2O_3 and SiO_2 having from 30 to 70% by weight of alumina and from 70 to 30% by weight of silica, preferably about equal parts by weight. The mixture can include other oxides such
30 as B_2O_3 , P_2O_5 , and ZrO_2 .

Melt-formed refractory ceramic fibers that can be used to make the heat-insulating mat are available from a number of commercial sources and include these known under the trade designation "Fiberfrax" from Carborundum Co., Niagara Falls, NY; "Cerafiber" and "Kaowool" from Thermal Ceramics Co., Augusta, GA; "Cer-wool" from Premier Refractories Co., Erwin, TN; and "SNSC" from Shin-Nippon Steel
35 Chemical of Tokyo, Japan. The manufacturer of ceramic fibers known under the trade designation "Cer-wool" states that they are melt-spun from a mixture of by weight 48% silica and 52% alumina and have an average fiber diameter of 3-4 micrometers. The manufacturer of ceramic fibers known under the trade designation "Cerafiber" states that they are melt-spun from a mixture of by weight 54% silica and 46% alumina and have an average fiber diameter of 2.5-3.5 micrometers. The manufacturer of ceramic fibers
40 "SNSC 1260-D1" states that they are melt-formed from a mixture of by weight 54% silica and 46% alumina and have an average fiber diameter of about 2 micrometers.

The individual ceramic fibers of the heat-insulating mat preferably are from 2 to 8 micrometers in diameter. If they were of substantially larger diameter, the mat would be more fragile and would require substantially more binder to afford adequate handlability. It is difficult to melt-form refractory ceramic fibers
45 at diameters smaller than 2 micrometers or larger than 8 micrometers.

The single figure of the drawing is a schematic central cross-section through a portion of an automotive exhaust system. Shown is a fragment of a catalytic converter that has a pair of insulated end cones, one of which is shown attached to an insulated exhaust pipe. Each of the catalytic converter, insulated end cone, and insulated exhaust pipe incorporates a mat of refractory ceramic fibers according to the invention.

50 In the drawing, a catalytic converter 10 includes a metallic casing having a cylindrical canister 12 that has been welded to a pair of insulated end cones of which only the inlet end cone 14 is shown. A metallic monolith 15 is mounted in the cylindrical canister 12 by a mat 16 of annealed refractory ceramic fibers. Each of the inlet and outlet end cones has an outer metal wall 18 and an inner metal wall 19, between which is a space filled with a mat 20 of annealed, melt-formed refractory ceramic fibers. At its opening, the
55 inlet end cone 14 is bolted to an insulated exhaust pipe 22 that has an outer metal wall 24, and an inner metal wall 25, between which is a space filled with a mat 26 of annealed, melt-formed refractory ceramic fibers.

TESTINGResiliency Test

5 A heat-insulating mat can be tested for Resiliency Value by being made to have a weight/area of 1610 g/m². A 2.5-cm disk of the mat is placed between two steel anvils at room temperature (R.T.). The anvils are closed to a 4.24 mm gap, and the pressure is recorded. The anvils are then heated so that the top anvil is at 800 °C and the bottom anvil is at 430 °C while simultaneously reducing the gap to 3.99 mm. After recording the pressure, the heaters are shut off, allowing both anvils to cool back to room temperature while
 10 adjusting the gap back to the original 4.24 mm, thus simulating conditions to which a mat is subjected when used to mount a metallic monolith in a catalytic converter. A recorded pressure, which is the Resiliency Value of the test mat, of at least 10 kPa indicates that the tested mat should have sufficient resiliency to be used for mounting a metallic monolith in a canister of a catalytic converter. By having such resiliency, the mat should keep a metallic monolith securely in place in a catalytic converter. The Resiliency Value
 15 preferably is at least 20 kPa, more preferably at least 50 kPa, to provide greater assurance that a metallic monolith will not become loose during the projected useful life of a catalytic converter.

Hot-shake Test

20 A heat-insulating mat is used to mount in the canister of a catalytic converter a metallic monolith that is 9 cm in diameter and 7.6 cm in length. Exhaust gases are passed through the converter while simultaneously subjecting it to mechanical vibration to simulate vibrations that would be encountered in vehicular use. Using an electromechanical vibrator made by Unholtz-Dickie Corp, an acceleration of 40 g's at 100 Hz frequency is applied to the converter. The heat source is a natural gas burner that supplies to the converter
 25 an inlet gas temperature of 800 °C. The gas temperature is cycled in order to test the ability of the mounting mat to maintain its resiliency and corresponding holding force while the space it occupies is changing dimensions. One cycle consists of 10 minutes at 800 °C and 10 minutes with the gas burner shut off. Vibration is maintained throughout the test. The duration of the test is 20 cycles if there is no earlier failure.
 30 In each of the examples, all parts are given by weight.

Examples 1-5

35 A number of commercially available refractory ceramic fibers were formed into mats by conventional wet-laid paper making. The mats were annealed in a muffle furnace as indicated in Table I, except that the fibers of Examples 2A, 4A, and 4B were annealed before being formed into a mat. Table I also indicates approximate shot contents. Before being annealed, the fibers of those mats of Table I with shot contents below 45% had been treated to reduce their shot content. Each mat had a weight/area of 1610 g/m² and contained about 5% organic binder before being annealed.

40 The three right-hand columns of Table I report results of the above-described "Resiliency Test", and the far right-hand column reports "Resiliency Values" obtained after both anvils had been returned to room temperature and the gap had been returned to 4.24 mm.

Table I also reports testing of mats of the same commercially available fibers that were not annealed and are called Comparative Examples 1X, 2X, 3X, 4X and 5X. As indicated by x-ray diffraction, the fibers of
 45 all of the mats of Table I were amorphous. TEM showed that the ceramic fibers known by the trade designation "Cerafiber" of Example 4C had some microcrystallinity, but was not used to test fibers of the other examples. TEM showed that when fibers known by the trade designation "Cer-wool" HP (57% shot content) were annealed at 900 °C for 72 hours, only a few of the fibers contained microcrystallinity whereas a majority of the fibers were amorphous.

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Table I

Example	Shot content (%)	Annealing		Pressure (kPa) when		
		temp. (°C)	time (min)	R.T./R.T. 4.24mm gap	800°C/430°C 3.99mm gap	T.T./R.T. 4.24mm gap
1A "Cer-wool" HP	33	950	120	144.8	155.1	65.5
1B "Cer-wool" HP	33	900	120	NT	NT	NT
1X "Cer-wool" HP	33	none		137.9	34.5	6.9
2A "Cer-wool" HP	45	700	8	227.5	69.0	20.7
2B "Cer-wool" HP	45	800	120	134.5	137.9	51.7
2C "Cer-wool" HP	45	970	300	89.5	131.0	51.7
2X "Cer-wool" HP	45	none		29.0	11.7	0
3A "Cer-wool" HP	57	800	120	34.5	58.0	23.0
3B "Cer-wool" HP	57	970	300	42.1	63.4	25.3
3X "Cer-wool" HP	57	none		15.9	5.9	0
4A "Cerafiber" VFS	33	700	8	172.5	64.0	27.6
4B "Cerafiber" VFS	33	950	120	117.3	120.8	41.4
4C "Cerafiber" VFS	33	800	120	NT	NT	NT
4X "Cerafiber" VFS	33	none		75.8	27.6	0
5A "SNSC" 1260 D-1 6	6	950	120	158.6	103.4	48.3
5X "SNSC" 1260 D-1 6	6	none		158.6	55.2	6.9

NT = not tested

As reported in Table I, the mats of each of Examples 1 - 5 had Resiliency Values greater than 20 kPa, whereas those of each of the Comparative Example were less than 10 kPa.

Portions of some of the mats of Table I were subjected to the above described Hot-shake Test at mount densities indicated in Table II.

Table II

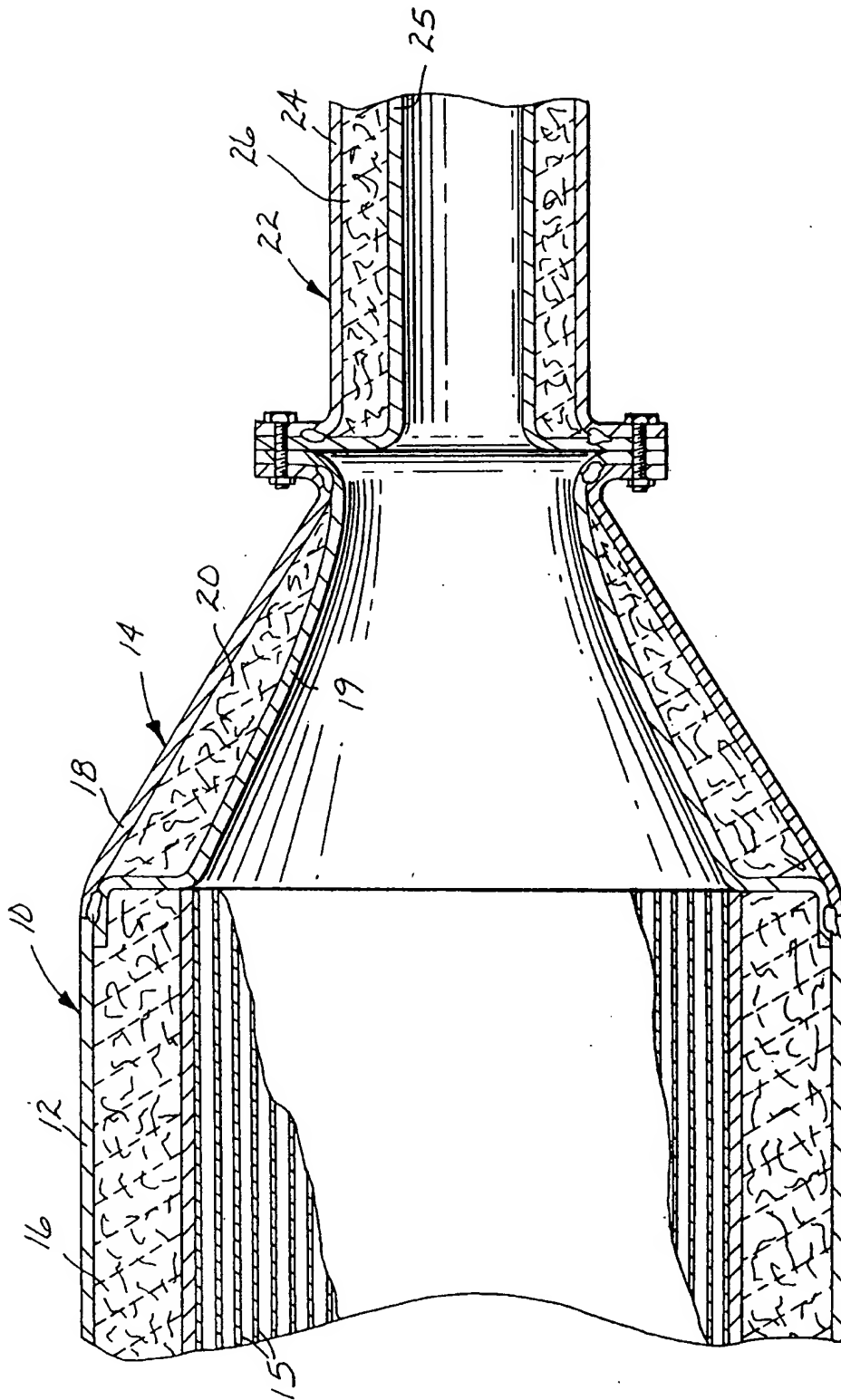
Example	Shot content (%)	Annealing		Mount Density (g/m ³)	Results (Hot-shake Test)
		temp. (°C)	time (min)		
1B "Cer-wool" HP	33	900	120	0.43	Fail 18 cycles
1X "Cer-wool" HP	33	none		0.62	Fail 1 cycle
2A "Cer-wool" HP	45	700	8	0.62	Fail 9 cycles
4A "Cerafiber" VFS	33	700	8	0.43	Pass 20 cycles
4C "Cerafiber" VFS	33	800	120	0.38	Fail 6 cycles
4C "Cerafiber" VFS	33	800	120	0.57	Pass 20 cycles
4X "Cerafiber" VFS	33	none		0.78	Fail 1 cycle

A mat at higher mount density normally provides a higher holding force and (consistent with a comparison between the two mount densities of 4C) allows a mat to withstand a larger number of cycles in the Hot-shake Test. In spite of the relatively high mount density of Comparative Examples 1X and 4X, each failed in the first cycle of the Hot-shake Test.

Claims

1. A catalytic converter including a monolith mounted in a canister by a heat-insulating mat characterized in that the mat comprises melt-formed refractory ceramic fibers that have been annealed at a temperature and for a time sufficient to provide a Resiliency Value of the mat of at least 10 kPa.
2. A catalytic converter as defined in claim 1 further characterized by the refractory ceramic fibers of the heatinsulating mat having a fine-grained crystalline form.
3. A catalytic converter as defined in claim 1 further characterized by the refractory ceramic fibers of the heat-insulating mat being substantially amorphous.
4. A catalytic converter as defined in claim 3 wherein the refractory ceramic fibers having been annealed at a temperature of at least 700 °C and less than 990 °C.
5. A catalytic converter as defined in claim 1 further characterized by the monolith being metallic.
6. A catalytic converter as defined in claim 1, further characterized by the heat-insulating mat containing additional heat-insulating materials selected from fibers and flakes.
7. A catalytic converter as defined in claim 6 further characterized by said additional heat-insulating materials forming a separate layer.
8. A catalytic converter as defined in claim 6 further characterized by said additional heat-insulating materials comprising unexpanded vermiculite flakes.
9. A device comprising a housing containing an inner metallic member that is insulated from the housing by a mat of ceramic fibers, which metallic member becomes hot in use and expands to compress the mat between the metallic member and the housing, said device being characterized by the feature that:

the mat primarily comprises melt-formed refractory ceramic fibers that have been annealed at a temperature and for a time sufficient to provide a Resiliency Value (as herein defined) of at least 10 kPa.





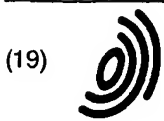
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EUROPEAN SEARCH REPORT

Application Number

EP 93 10 8273

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
Y	EP-A-0 328 293 (MINNESOTA MINING AND MANUFACTURING CO.) * the whole document *	1-9	C04B35/00 F01N3/28 C03C13/04
Y	EP-A-0 205 704 (ISOLITE BABCOCK REFRACTORIES CO., LTD.) * page 3, line 26 - page 5, line 26; claims; examples *	1-9	
A	EP-A-0 007 485 (THE CARBORUNDUM CO.) * page 7, line 4 - page 8, line 23; claims *	1,2,4,9	
A	GAS WÄRME INTERNATIONAL vol. 30, no. 7-8, 1981, pages 357 - 362 A.VON ESCHER 'CERAMIC FIBRES WITH ALUMINIUM OXIDE CONTENTS OF 45 UP TO 95% AND THEIR HIGH TEMPERATURE BEHAVIOUR' * page 359, left column, line 1, paragraph 2 - right column, line 1, paragraph 1; figure 10 *		TECHNICAL FIELDS SEARCHED (Int. Cl.5)
A	US-A-4 087 039 (R.N.BALLUFF)		C04B C03C F01N
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 17 SEPTEMBER 1993	Examiner HARBON J.L.
CATEGORY OF CITED DOCUMENTS			
X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	



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(12) **EUROPEAN PATENT SPECIFICATION**

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(22) Date of filing: **21.05.1993**

(54) **Catalytic converter having a metallic monolith mounted by a heat-insulating mat of refractory ceramic fibers**

Katalytischer Konverter mit einem metallischen Monolith, der von einer wärmedämmenden Matte aus feuerfesten Keramikfasern gehalten wird

Convertisseur catalytique ayant un monolithe métallique porté par un matelas de fibres céramiques réfractaires thermiquement isolant

(84) Designated Contracting States:
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(56) References cited:
EP-A- 0 007 485 EP-A- 0 205 704
EP-A- 0 328 293 US-A- 4 087 039

- **GAS WÄRME INTERNATIONAL** vol. 30, no. 7-8,
1981, pages 357 - 362, A.VON ESCHER 'CERAMIC
FIBRES WITH ALUMINIUM OXIDE CONTENTS OF
45 UP TO 95% AND THEIR HIGH TEMPERATURE
BEHAVIOUR'

Note: Within nine months from the publication of the mention of the grant of the European patent, any person may give notice to the European Patent Office of opposition to the European patent granted. Notice of opposition shall be filed in a written reasoned statement. It shall not be deemed to have been filed until the opposition fee has been paid. (Art. 99(1) European Patent Convention).

EP 0 573 834 B1

Description

The invention concerns a catalytic converter which has a metallic monolith that is mounted by a heat-insulating blanket or mat of refractory ceramic fibers. More generally, the invention is concerned with any device that has a canister containing a metallic member and a heat-insulating blanket between the metallic member and the canister.

A catalytic converter typically has a metallic or ceramic monolith which is mounted within a metal canister by a heat-insulating blanket. The blanket typically is a mat of refractory ceramic fibers. In use, the monolith is heated to temperatures on the order of 600° - 1000°C while the heat-insulating mat keeps the canister at much lower temperatures. This temperature differential causes a metallic monolith to expand more than the canister, thus narrowing the gap between the monolith and the canister and compressing the heat-insulating mat. Unless the mat is resilient, it can take such a compression set that the metallic monolith becomes loose when the catalytic converter cools. This would not only reduce the heat-insulating value of the mat, but in vehicular use, a loose monolith would produce annoying noises and by being buffeted would be subject to premature failure.

In addition to catalytic converters, there are other devices wherein a canister or other housing contains a metallic member that becomes hot and must be insulated from the housing by a blanket or mat of refractory ceramic fibers, e.g., a diesel particulate trap, an insulated end-cone, or an insulated doublewalled exhaust pipe such as that of coassigned U.S. Pat. No. 5,024,289 (Merry). Any such heat-insulating blanket or mat should be sufficiently resilient that it does not become loose by taking a compression set when the inner metallic member expands in use to narrow the gap between the inner metallic member and its housing.

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More broadly, a heat-insulating mat of annealed melt-formed refractory ceramic fibers can be employed to insulate any inner metallic member that becomes hot in use and expands to compress the mat between the metallic member and a housing.

The melt-formed refractory ceramic fibers of the heat-insulating mat can be annealed to develop a fine-grained crystalline form (as in the Johnson UK Pat. Spec.) while avoiding higher temperatures that would result in a coarse-grained structure and consequently result in an unsatisfactory Resiliency Value. However, by restricting the annealing temperature and time such that the melt-formed fibers remain substantially amorphous, there is a significant energy saving as compared to Johnson's need to develop a crystalline structure.

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up to about 60% by weight of the heat-insulating mat. However, lower levels of shot are preferred when available at equivalent costs.

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A binder can be avoided by wet-laying the fibers to align most of the fibers in the plane of the heat-insulating mat, but such a mat can be difficult to handle.

The heat-insulating mat can contain additional fibers, flakes and other materials that are heat-insulating as long as they are used in proportions that do not reduce the Resiliency Value to less than 10 kPa. In addition to or instead of being contained within the heat-insulating mat, such other materials can form a separate layer similar to the intumescent sheet material 32 of Fig. 3 of the Merry '429 patent. Such additional materials include unexpanded vermiculite flakes and other materials listed at col. 3, lines 28-48 of Merry '429.

A useful heat-insulating mat can be made from about 1 to 70% by weight of intumescent material, about 10 to 70% by weight of annealed melt-formed refractory ceramic fibers, and about 3 to 20% by weight of binder.

The melt-formed refractory ceramic fibers can be melt-blown or melt-spun from a variety of metal oxides, preferably a mixture of Al_2O_3 and SiO_2 having from 30 to 70% by weight of alumina and from 70 to 30% by weight of silica, preferably about equal parts by weight. The mixture can include other oxides such as B_2O_3 , P_2O_5 , and ZrO_2 .

Melt-formed refractory ceramic fibers that can be used to make the heat-insulating mat are available from a number of commercial sources and include these known under the trade designation "Fiberfrax" from Carborundum Co., Niagara Falls, NY; "Cerafiber" and "Kaowool" from Thermal Ceramics Co., Augusta, GA; "Cer-wool" from Premier Refractories Co., Erwin, TN; and "SNSC" from Shin-Nippon Steel Chemical of Tokyo, Japan. The manufacturer of ceramic fibers known under the trade designation "Cer-wool" states that they are melt-spun from a mixture of by weight 48% silica and 52% alumina and have an average fiber diameter of 3-4 micrometers. The manufacturer of ceramic fibers known under the trade designation "Cerafiber" states that they are melt-spun from a mixture of by weight 54% silica and 46% alumina and have an average fiber diameter of 2.5-3.5 micrometers. The manufacturer of ceramic fibers "SNSC 1260-D1" states that they are melt-formed from a mixture of by weight 54% silica and 46% alumina and have an average fiber diameter of about 2 micrometers.

The individual ceramic fibers of the heat-insulating mat preferably are from 2 to 8 micrometers in diameter. If they were of substantially larger diameter, the mat would be more fragile and would require substantially more binder to afford adequate handability. It is difficult to melt-form refractory ceramic fibers at diameters smaller than 2 micrometers or larger than 8 micrometers.

The single figure of the drawing is a schematic central cross-section through a portion of an automotive exhaust system. Shown is a fragment of a catalytic converter that has a pair of insulated end cones, one of which is shown attached to an insulated exhaust pipe. Each of the catalytic converter, insulated end cone, and insulated exhaust pipe incorporates a mat of refractory ceramic fibers according to the invention.

In the drawing, a catalytic converter 10 includes a metallic casing having a cylindrical canister 12 that has been welded to a pair of insulated end cones of which only the inlet end cone 14 is shown. A metallic monolith 15 is mounted in the cylindrical canister 12 by a mat 16 of annealed refractory ceramic fibers. Each of the inlet and outlet end cones has an outer metal wall 18 and an inner metal wall 19, between which is a space filled with a mat 20 of annealed, melt-formed refractory ceramic fibers. At its opening, the inlet end cone 14 is bolted to an insulated exhaust pipe 22 that has an outer metal wall 24, and an inner metal wall 25, between which is a space filled with a mat 26 of annealed, melt-formed refractory ceramic fibers.

TESTING

Resiliency Test

A heat-insulating mat can be tested for Resiliency Value by being made to have a weight/area of 1610 g/m². A 2.5-cm disk of the mat is placed between two steel anvils at room temperature (R.T.). The anvils are closed to a 4.24 mm gap, and the pressure is recorded. The anvils are then heated so that the top anvil is at 800°C and the bottom anvil is at 430°C while simultaneously reducing the gap to 3.99 mm. After recording the pressure, the heaters are shut off, allowing both anvils to cool back to room temperature while adjusting the gap back to the original 4.24 mm, thus simulating conditions to which a mat is subjected when used to mount a metallic monolith in a catalytic converter. A recorded pressure, which is the Resiliency Value of the test mat, of at least 10 kPa indicates that the tested mat should have sufficient resiliency to be used for mounting a metallic monolith in a canister of a catalytic converter. By having such resiliency, the mat should keep a metallic monolith securely in place in a catalytic converter. The Resiliency Value pref-

erably is at least 20 kPa, more preferably at least 50 kPa, to provide greater assurance that a metallic monolith will not become loose during the projected useful life of a catalytic converter.

Hot-shake Test

A heat-insulating mat is used to mount in the canister of a catalytic converter a metallic monolith that is 9 cm in diameter and 7.6 cm in length. Exhaust gases are passed through the converter while simultaneously subjecting it to mechanical vibration to simulate vibrations that would be encountered in vehicular use. Using an electromechanical vibrator made by Unholtz-Dickie Corp, an acceleration of 40 g's at 100 Hz frequency is applied to the converter. The heat source is a natural gas burner that supplies to the converter an inlet gas temperature of 800°C. The gas temperature is cycled in order to test the ability of the mounting mat to maintain its resiliency and corresponding holding force while the space it occupies is changing dimensions. One cycle consists of 10 minutes at 800°C and 10 minutes with the gas burner shut off. Vibration is maintained throughout the test. The duration of the test is 20 cycles if there is no earlier failure.

In each of the examples, all parts are given by weight.

Examples 1-5

A number of commercially available refractory ceramic fibers were formed into mats by conventional wet-laid paper making. The mats were annealed in a muffle furnace as indicated in Table I, except that the fibers of Examples 2A, 4A, and 4B were annealed before being formed into a mat. Table I also indicates approximate shot contents. Before being annealed, the fibers of those mats of Table I with shot contents below 45% had been treated to reduce their shot content. Each mat had a weight/area of 1610 g/m² and contained about 5% organic binder before being annealed.

The three right-hand columns of Table I report results of the above-described "Resiliency Test", and the far right-hand column reports "Resiliency Values" obtained after both anvils had been returned to room temperature and the gap had been returned to 4.24 mm.

Table I also reports testing of mats of the same commercially available fibers that were not annealed and are called Comparative Examples 1X, 2X, 3X, 4X and 5X. As indicated by x-ray diffraction, the fibers of all of the mats of Table I were amorphous. TEM showed that the ceramic fibers known by the trade designation "Cerafiber" of Example 4C had some microcrystallinity, but was not used to test fibers of the other examples. TEM showed that when fibers known by the trade designation "Cer-wool" HP (57% shot content) were annealed at 900°C for 72 hours, only a few of the fibers contained microcrystallinity whereas a majority of the fibers were amorphous.

Table I

	Example	Shot content (%)	Annealing		Pressure (Pa) when		
			temp. (°C)	time (min)	R.T./R.T. 4.24mm gap	800°C/430°C 3.99mm gap	T.T./R.T. 4.24mm gap
5	1A "Cer-wool" HP	33	950	120	144.8	155.1	65.5
	1B "Cer-wool" HP	33	900	120	NT	NT	NT
10	1X "Cer-wool" HP	33	none		137.9	34.5	6.9
	2A "Cer-wool" HP	45	700	8	227.5	69.0	20.7
	2B "Cer-wool" HP	45	800	120	134.5	137.9	51.7
	2C "Cer-wool" HP	45	970	300	89.5	131.0	51.7
15	2X "Cer-wool" HP	45	none		29.0	11.7	0
	3A "Cer-wool" HP	57	800	120	34.5	58.0	23.0
	3B "Cer-wool" HP	57	970	300	42.1	63.4	25.3
20	3X "Cer-wool" HP	57	none		15.9	5.9	0
	4A "Cerafiber" VFS	33	700	8	172.5	64.0	27.6
	4B "Cerafiber" VFS	33	950	120	117.3	120.8	41.4
	4C "Cerafiber" VFS	33	800	120	NT	NT	NT
25	4X "Cerafiber" VFS	33	none		75.8	27.6	0
	5A "SNSC" 1260 D-1	6	950	120	158.6	103.4	48.3
	5X "SNSC" 1260 D-1	6	none		158.6	55.2	6.9
30	NT = not tested						

As reported in Table I, the mats of each of Examples 1 - 5 had Resiliency Values greater than 20 kPa, whereas those of each of the Comparative Example were less than 10 kPa.

Portions of some of the mats of Table I were subjected to the above described Hot-shake Test at mount densities indicated in Table II.

Table II

Example	Shot content (%)	Annealing		Mount Density (g/m ³)	Results (Hot-shake Test)
		temp. (°C)	time (min)		
1B "Cer-wool" HP	33	900	120	0.43	Fail 18 cycles
1X "Cer-wool" HP	33	none		0.62	Fail 1 cycle
2A "Cer-wool" HP	45	700	8	0.62	Fail 9 cycles
4A "Cerafiber" VFS	33	700	8	0.43	Pass 20 cycles
4C "Cerafiber" VFS	33	800	120	0.38	Fail 6 cycles
4C "Cerafiber" VFS	33	800	120	0.57	Pass 20 cycles
4X "Cerafiber" VFS	33	none		0.78	Fail 1 cycle

A mat at higher mount density normally provides a higher holding force and (consistent with a comparison between the two mount densities of 4C) allows a mat to withstand a larger number of cycles in the Hot-shake Test. In spite of the relatively high mount density of Comparative Examples 1X and 4X, each failed in the first cycle of the Hot-shake Test.

Claims

1. A catalytic converter including a monolith mounted in a canister by a heat-insulating mat characterized in that the mat comprises melt-formed refractory ceramic fibers that have been annealed at a temperature and for a time sufficient to provide a Resiliency Value of the mat of at least 10 kPa.
2. A catalytic converter as defined in claim 1 further characterized by the refractory ceramic fibers of the heatinsulating mat having a fine-grained crystalline form.
3. A catalytic converter as defined in claim 1 further characterized by the refractory ceramic fibers of the heat-insulating mat being substantially amorphous.
4. A catalytic converter as defined in claim 3 wherein the refractory ceramic fibers having been annealed at a temperature of at least 700°C and less than 990°C.
5. A catalytic converter as defined in claim 1 further characterized by the monolith being metallic.
6. A catalytic converter as defined in claim 1, further characterized by the heat-insulating mat containing additional heat-insulating materials selected from fibers and flakes.
7. A catalytic converter as defined in claim 6 further characterized by said additional heat-insulating materials forming a separate layer.
8. A catalytic converter as defined in claim 6 further characterized by said additional heat-insulating materials comprising unexpanded vermiculite flakes.
9. A device comprising a housing containing an inner metallic member that is insulated from the housing by a mat of ceramic fibers, which metallic member becomes hot in use and expands to compress the mat between the metallic member and the housing, said device being characterized by the feature that:
the mat primarily comprises melt-formed refractory ceramic fibers that have been annealed at a temperature and for a time sufficient to provide a Resiliency Value (as herein defined) of at least 10 kPa.

Patentansprüche

1. Katalysator, umfassend einen Monolithen, der in einem Gehäuse durch eine wärmedämmende Matte gehalten wird, dadurch gekennzeichnet, daß die Matte schmelzgeformte, feuerfeste Keramikfasern umfaßt, die bei einer Temperatur und über einen Zeitraum geglüht wurden, die ausreichen, der Matte einen Elastizitätswert von wenigstens 10kPa zu verleihen.
2. Katalysator nach Anspruch 1, ferner dadurch gekennzeichnet, daß die feuerfesten Keramikfasern der wärmedämmenden Matte eine feinkörnige kristalline Form besitzen.
3. Katalysator nach Anspruch 1, ferner dadurch gekennzeichnet, daß die feuerfesten Keramikfasern der wärmedämmenden Matte im wesentlichen amorph sind.
4. Katalysator nach Anspruch 3, wobei die feuerfesten Keramikfasern bei einer Temperatur von wenigstens 700°C und weniger als 990°C geglüht wurden.
5. Katalysator nach Anspruch 1, ferner dadurch gekennzeichnet, daß der Monolith metallisch ist.
6. Katalysator nach Anspruch 1, ferner dadurch gekennzeichnet, daß die wärmedämmende Matte zusätzliche, wärmedämmende Materialien, gewählt aus Fasern und Flocken, enthält.
7. Katalysator nach Anspruch 6, ferner dadurch gekennzeichnet, daß die zusätzlichen, wärmedämmenden Materialien eine getrennte Schicht bilden.
8. Katalysator nach Anspruch 6, ferner dadurch gekennzeichnet, daß die zusätzlichen, wärmedämmenden Materialien nicht-expandierte Vermiculitflocken umfassen.

9. Vorrichtung, umfassend ein Gehäuse, das ein metallisches Innenteil, welches durch eine Matte aus keramischen Fasern vom Gehäuse gedämmt ist, enthält, wobei das metallische Teil bei Gebrauch heiß wird und sich ausdehnt, wodurch die Matte zwischen dem metallischen Teil und dem Gehäuse zusammengedrückt wird, wobei diese Vorrichtung durch das Merkmal gekennzeichnet ist, daß

5 die Matte in erster Linie schmelzgeformte feuerfeste Keramikfasern umfaßt, die bei einer Temperatur und über eine Dauer gegläht wurden, die ausreichen, einen Elastizitätswert (wie hier definiert) von wenigstens 10 kPa zu verleihen.

Revendications

- 10 1. Convertisseur catalytique comprenant un monolithe porté, à l'intérieur d'une boîte métallique, par un mat thermiquement isolant caractérisé en ce que le mat est constitué de fibres céramiques réfractaires formées au fondu qui ont été recuites à une température et pendant un temps suffisants pour fournir une valeur de résilience du mat d'au moins 10 kPa.
- 15 2. Convertisseur catalytique selon la revendication 1, caractérisé en plus en ce que les fibres céramiques réfractaires du mat thermiquement isolant ont une forme cristalline à grains fins.
3. Convertisseur catalytique selon la revendication 1, caractérisé en plus en ce que les fibres céramiques réfractaires du mat thermiquement isolant sont essentiellement amorphes.
- 20 4. Convertisseur catalytique selon la revendication 3, dans lequel les fibres céramiques réfractaires sont recuites à une température d'au moins 700°C et inférieure à 990°C.
- 25 5. Convertisseur catalytique selon la revendication 1, caractérisé en plus en ce que le monolithe est métallique.
6. Convertisseur catalytique selon la revendication 1, caractérisé en plus en ce que le mat thermiquement isolant contient d'autres matériaux thermiquement isolants choisis parmi les fibres et les flocons.
- 30 7. Convertisseur catalytique selon la revendication 6, caractérisé en plus en ce que lesdits autres matériaux thermiquement isolants forment une couche séparée.
8. Convertisseur catalytique selon la revendication 6, caractérisé en plus en ce que lesdits autres matériaux thermiquement isolants comprennent des flocons de vermiculite non-expansée.
- 35 9. Dispositif comprenant un carter contenant un élément métallique interne qui est isolé du carter par un mat de fibres céramiques, lequel élément métallique devient chaud en utilisation et se dilate pour comprimer le mat entre l'élément métallique et le carter, ledit dispositif étant caractérisé en ce que :
- 40 le mat est essentiellement composé de fibres céramiques réfractaires formées au fondu qui ont été recuites à une température et pendant un temps suffisants pour fournir une valeur de résilience (telle que définie dans la présente) d'au moins 10 kPa.
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